

1. Prove spectrum properties(N is WSS) :

- (1) $R_{N_i}(\tau) = R_{N_o}(\tau)$ and $R_{N_i, N_o}(\tau) = -R_{N_o, N_i}(\tau)$
- (2) $R_N(\tau) = R_{N_i}(\tau)\cos(2\pi f_c\tau) - R_{N_o, N_i}(\tau)\sin(2\pi f_c\tau)$
- (3) $R_{\tilde{N}}(\tau) = R_{N_i}(\tau) + jR_{N_o, N_i}(\tau)$
- (4) $R_N(\tau) = \text{Re}\{R_{\tilde{N}}(\tau)\exp(j2\pi f_c\tau)\}$
- (5) $S_{\tilde{N}}(f)$ is real valued.
- (6) $S_{N_i}(f) = S_{N_o}(f)$ and $S_{N_i, N_o}(f) = -S_{N_o, N_i}(f)$
- (7) $S_N(f) = \frac{1}{2}(S_{\tilde{N}}(f - f_c) + S_{\tilde{N}}(-f - f_c))$

Sol: 請參考講義 1-219~1-224.

2. Consider a square-law detector, using a nonlinear device whose transfer characteristic is defined by

$$v_2 = a_1v_1(t) + a_2v_1^2(t)$$

where a_1 and a_2 are constants, $v_1(t)$ is the input, and $v_2(t)$ is the output. The input consists of the AM wave

$$v_1(t) = A_c[1 + k_a m(t)]\cos(2\pi f_c t)$$

- (1) Evaluate the output $v_2(t)$.
- (2) Find the conditions for which the message signal $m(t)$ may be recovered from $v_2(t)$.

Sol:

Let

$$v_1(t) = A_c[1 + k_a m(t)]\cos(2\pi f_c t)$$

(a) Then the output of the square-law device is

$$\begin{aligned} v_2(t) &= a_1v_1(t) + a_2v_1^2(t) \\ &= a_1A_c[1 + k_a m(t)]\cos(2\pi f_c t) \\ &\quad + \frac{1}{2}a_2A_c^2[1 + 2k_a m(t) + k_a^2 m^2(t)] [1 + \cos(4\pi f_c t)] \end{aligned}$$

- (b) The desired signal, namely $a_2A_c^2k_a^2m(t)$, is due to the $a_2v_1^2(t)$ - hence, the name "square-law detection". This component can be extracted by means of a low-pass filter. This is not the only contribution within the baseband spectrum, because the term $1/2 a_2A_c^2k_a^2m^2(t)$ will give rise to a plurality of similar frequency components. The ratio of wanted signal to distortion is $2/k_a m(t)$. To make this ratio large, the percentage modulation, that is, $|k_a m(t)|$ should be kept small compared with unity.