

1. An unmodulated carrier of amplitude A_c and frequency f_c and band-limited white noise are summed and then passed through an ideal envelope detector. Assume the noise spectral density to be of height $N_0/2$ and bandwidth $2W$, centered about the carrier frequency f_c . Determine the output signal-to-noise ratio for the case when the carrier-to-noise ratio is high.

Sol:

The received signal is

$$\begin{aligned} x(t) &= A_c \cos(2\pi f_c t) + n(t) \\ &= A_c \cos(2\pi f_c t) + n_c(t) \cos(2\pi f_c t) - n_s(t) \sin(2\pi f_c t) \\ &= [A_c + n_c(t)] \cos(2\pi f_c t) - n_s(t) \sin(2\pi f_c t) \end{aligned}$$

The envelope detector output is therefore

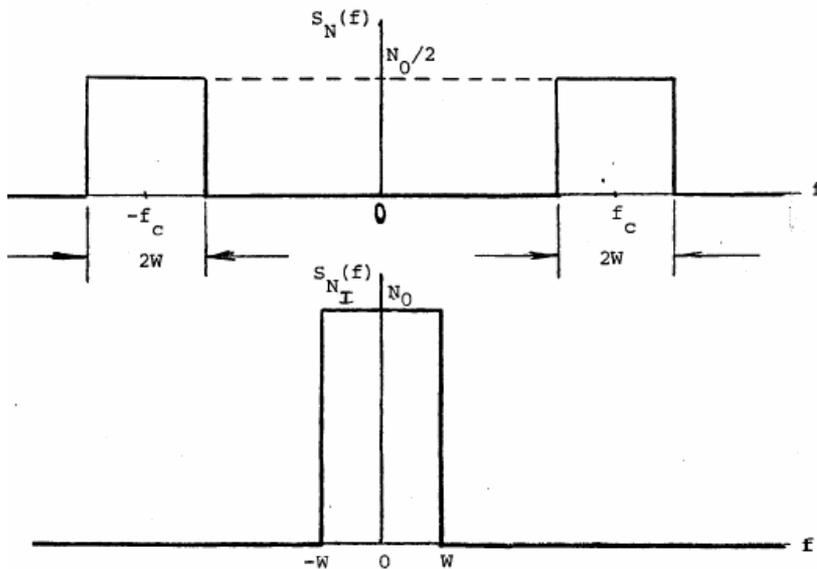
$$a(t) = \{[A_c + n_c(t)]^2 + n_s^2(t)\}^{1/2}$$

For the case when the carrier-to-noise ratio is high, we may approximate this result as

$$a(t) \approx A_c + n_c(t)$$

The term A_c represents the useful signal component. The output signal power is thus A_c^2 .

The power spectral densities of $n(t)$ and $n_s(t)$ are as shown below:



The output noise power is $2N_0W$. The output signal-to-noise ratio is therefore

$$(\text{SNR})_0 = \frac{A_c^2}{2N_0W}$$

2. Suppose that the received signal in FM system contains some residual amplitude modulation of positive amplitude $a(t)$, as shown by

$$s(t) = a(t) \cos[2\pi f_c t + \phi(t)]$$

Where f_c is the carrier frequency. The phase $\phi(t)$ is related to the modulating signal $m(t)$ by

$$\phi(t) = 2\pi k_f \int_0^t m(\tau) d\tau$$

Where k_f is a constant. Assume that the signal $s(t)$ is restricted to a frequency band of width B_T , centered at f_c , where B_T is the transmission bandwidth of the FM signal in the absence of amplitude modulation, and that the amplitude modulation is slowly varying compared with $\phi(t)$. Show that the output of an ideal frequency discriminator produced by $s(t)$ is proportional to $a(t)m(t)$. Hint: Use the complex notation described in Appendix 2 to represent the modulated wave $s(t)$.

Sol:

The complex envelope of the modulated wave $s(t)$ is

$$\tilde{s}(t) = a(t) \exp[j\phi(t)]$$

Since $a(t)$ is slowly varying compared to $\exp[j\phi(t)]$, the complex envelope $\tilde{s}(t)$ is restricted effectively to the frequency band $-B_T/2 \leq f \leq B_T/2$. An ideal frequency discriminator consists of a differentiator followed by an envelope detector. The output of the differentiator, in response to $\tilde{s}(t)$, is

$$\begin{aligned} \tilde{v}_o(t) &= \frac{d}{dt} \tilde{s}(t) \\ &= \frac{d}{dt} [a(t) \exp[j\phi(t)]] \\ &= \frac{da(t)}{dt} \exp[j\phi(t)] + j \frac{d\phi(t)}{dt} a(t) \exp[j\phi(t)] \\ &= a(t) \exp[j\phi(t)] \left[\frac{1}{a(t)} \frac{da(t)}{dt} + j \frac{d\phi(t)}{dt} \right] \end{aligned}$$

Since $a(t)$ is slowly varying compared to $\phi(t)$, we have

$$\left| \frac{d\phi(t)}{dt} \right| \gg \left| \frac{1}{a(t)} \frac{da(t)}{dt} \right|$$

Accordingly, we may approximate $\tilde{v}_o(t)$ as

$$\tilde{v}_o(t) \approx j a(t) \frac{d\phi(t)}{dt} \exp[j\phi(t)]$$

However, by definition

$$\phi(t) = 2\pi k_f \int_0^t m(t) dt$$

Therefore,

$$\tilde{v}_o(t) = j2\pi k_f a(t) m(t) \exp[j\phi(t)]$$

Hence, the envelope detector output is proportional to $a(t) m(t)$ as shown by

$$|\tilde{v}_o(t)| = 2\pi k_f a(t) m(t)$$

3. What are the definitions of SNR_i , SNR_o , SNR_c and figure of merit?

Input signal-to-noise ratio (SNR_I)

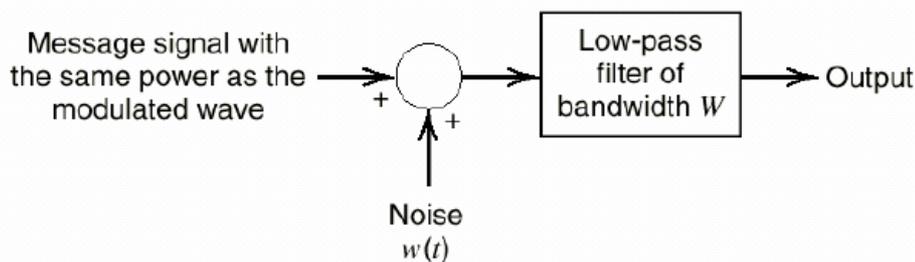
- The ratio of the average power of the modulated signal $s(t)$ to the average power of the filtered noise $n(t)$.

Output signal-to-noise ratio (SNR_O)

- The ratio of the average power of the demodulated message signal to the average power of the noise, measured at the receiver output.

Channel signal-to-noise ratio (SNR_C)

- The ratio of the average power of the modulated signal $s(t)$ to the average power of the channel noise in the message bandwidth, measured at the receiver input (as illustrated below).



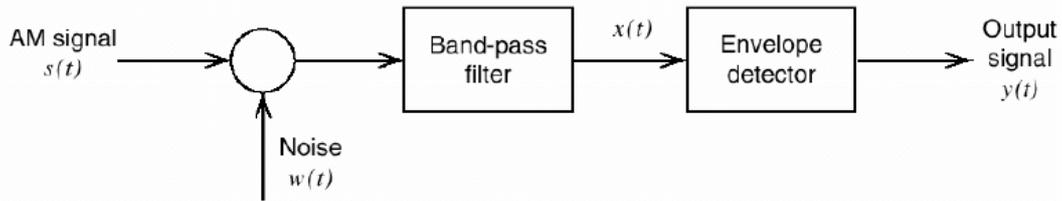
$$\text{figure of merit} = \frac{SNR_O}{SNR_C}$$

4. In a full AM signal, both sidebands and the carrier wave are transmitted, as shown by

$$s(t) = A_c[1 + k_a m(t)] \cos(2\pi f_c t)$$

where $A_c \cos(2\pi f_c t)$ is the carrier wave, $m(t)$ is the message signal, and k_a is a constant that determines the percentage modulation. Please compute the SNR_C for this AM signal $s(t)$. (Note: assume $m(t)$ is zero mean and the message bandwidth is W .)

sol:



$$s(t) = A_c[1 + k_a m(t)] \cos(2\pi f_c t)$$

$$\begin{aligned} \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T E[s^2(t)] dt &= A_c^2 E[(1 + k_a m(t))^2] \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \cos^2(2\pi f_c t) dt \\ &= \frac{A_c^2}{2} (1 + k_a^2 P) \quad (\text{Assume } m(t) \text{ zero mean.}) \end{aligned}$$

$$\text{Also, } \int_{-W}^W S_w(f) df = \int_{-W}^W \frac{N_0}{2} df = WN_0$$

$$SNR_{C,AM} = \frac{A_c^2 (1 + k_a^2 P)}{2WN_0}$$